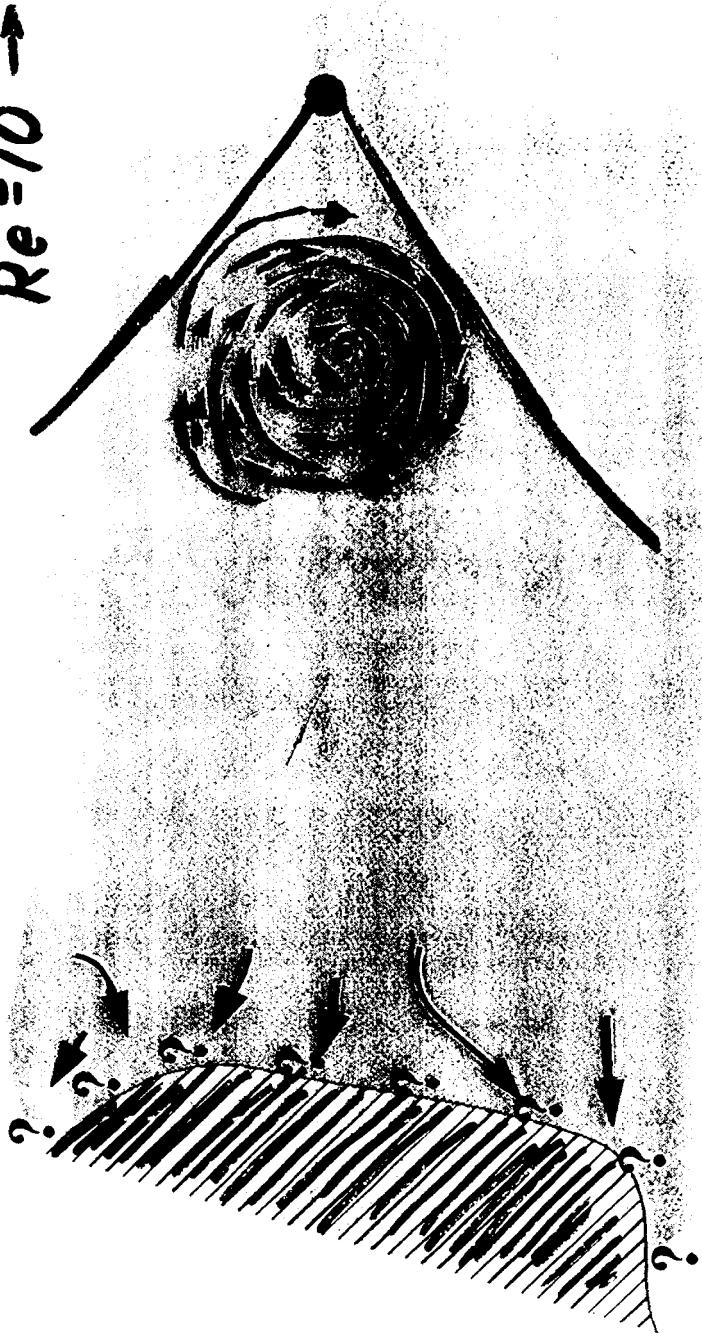


MODEL FOR PREDICTION

$$\frac{\partial v}{\partial t} + v \nabla v = -\frac{1}{\rho} \nabla p + v \nabla^2 v$$
$$\nabla \cdot v = 0$$

$$Re = 10^4 \rightarrow N = 10^{10}$$
$$Re = 10^6 \rightarrow N = 10^{13}$$

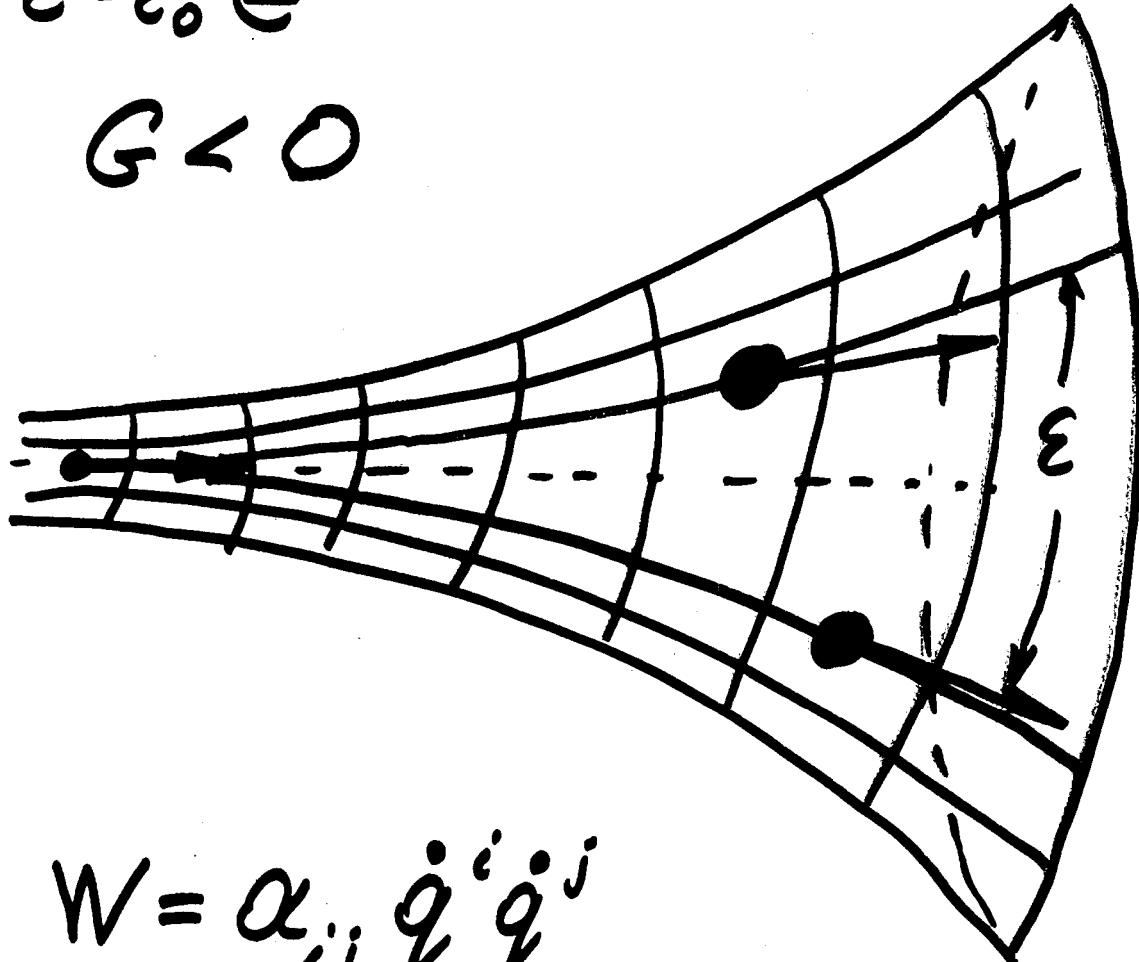


Instability and Unpredictable Solutions

1. Orbital Instability

$$\epsilon = \epsilon_0 e^{\sqrt{-G} t}$$

$$G < 0$$



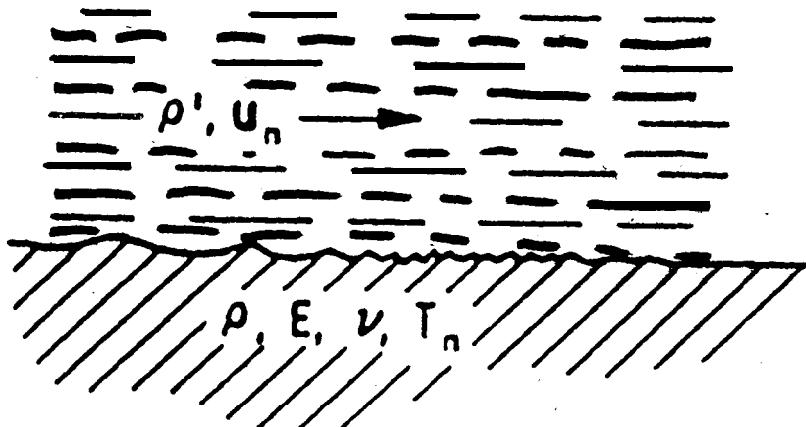
$$W = \alpha_{ij} \dot{q}^i \dot{q}^j$$

$$g_{ij} = \alpha_{ij}$$

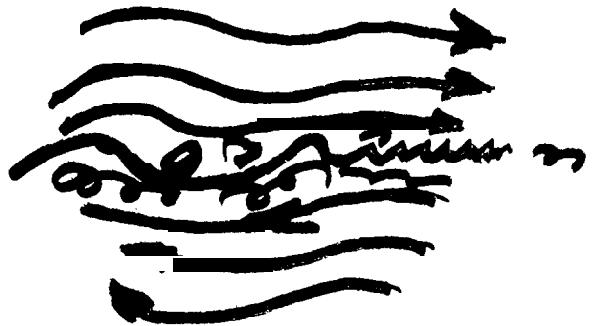
$$\begin{aligned}\frac{\partial L}{\partial \epsilon} &\equiv 0 \\ Q_\epsilon &\equiv 0\end{aligned}$$

Warping of Boundaries

$$T_{nn} < \frac{S_1 S_2}{(S_1 + S_2)^2} \gamma_n^2 - \frac{E}{2(1+\nu)}$$



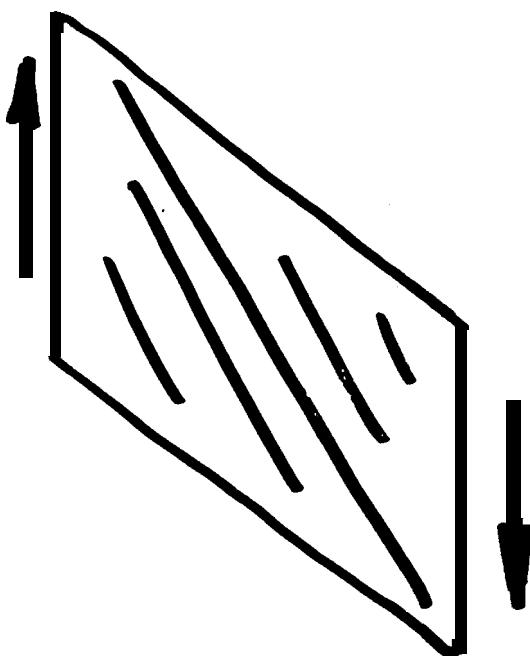
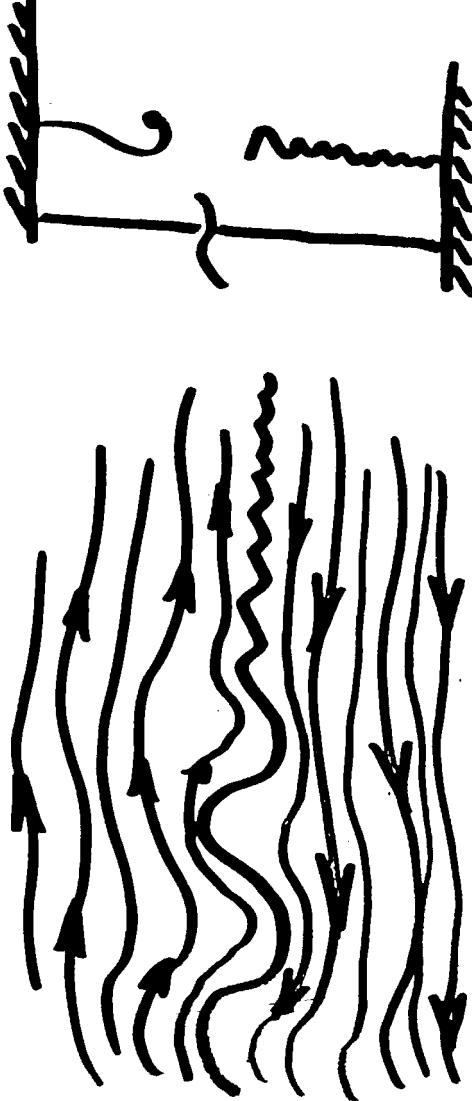
Eulerian Turbulence if $E \rightarrow 0$



$$\lambda = \frac{1}{2} (U_2 - U_1) (1 \pm i)$$

2. Hadamard's Instability (Failure of Hyperbolicity)

Instability

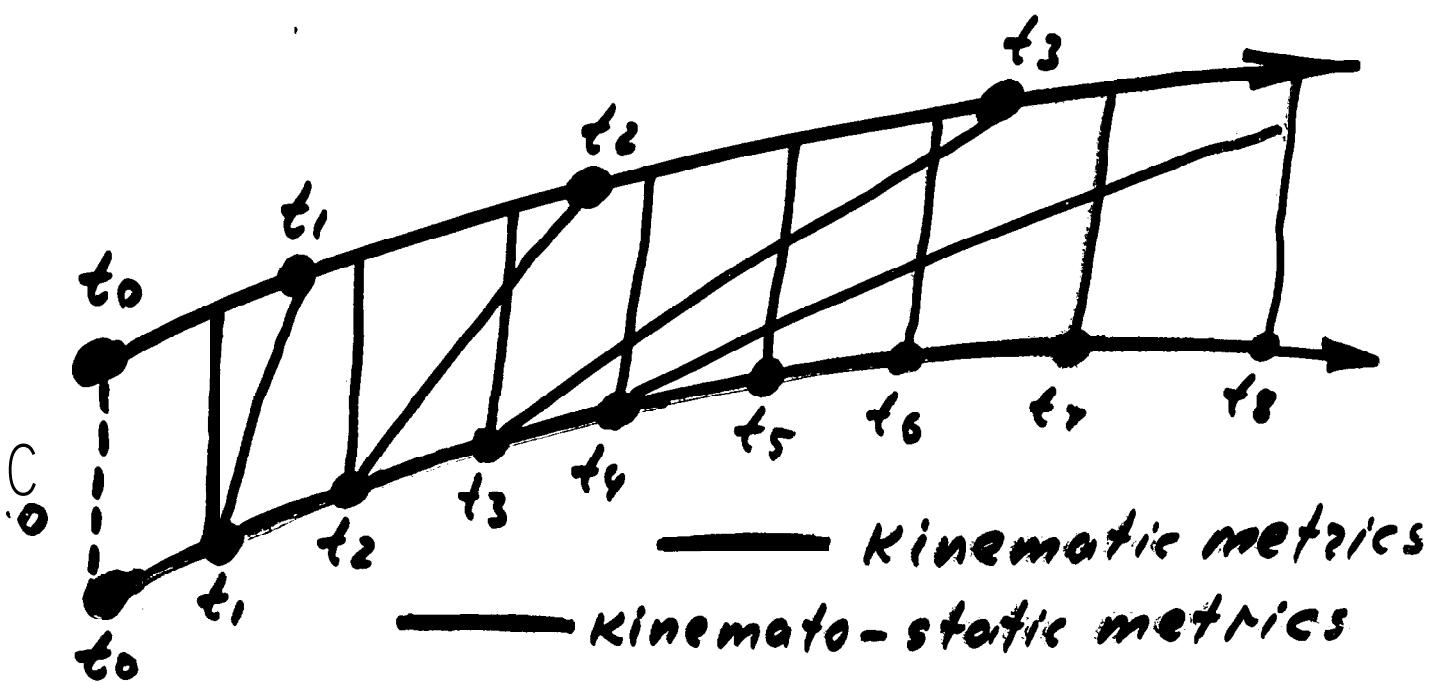


$$\frac{\partial^2 \theta}{\partial t^2} - \frac{2\pi c \theta}{n^2 e} = 0 \quad \lambda > 0$$

$$\frac{\partial^2 \theta}{\partial t^2} = 0 \quad \lambda = 0$$

Instability is not an invariant of motion

1. Instability and metrics of configuration space



$$\dot{\gamma} = -x + \frac{1}{2}y^2$$

$$x = \frac{1}{2}t^2 + At + B$$

$$y = C \sin(t + D)$$

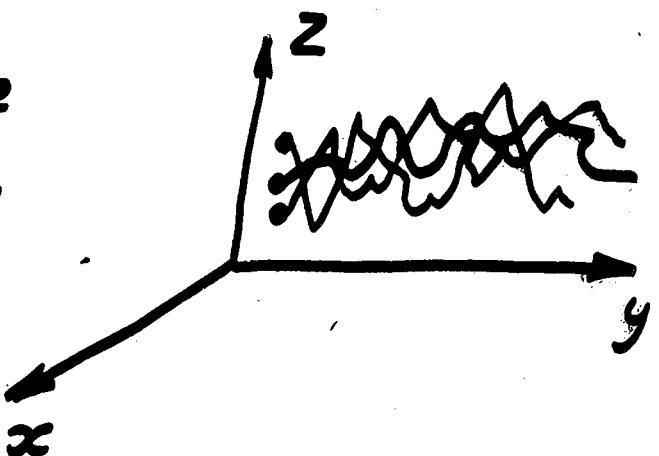
Unperturbed motion
 $x = \frac{1}{2}t^2 + t$, $y = 0$
 is stable in —
 and unstable in —

2. Instability and Frame of Reference

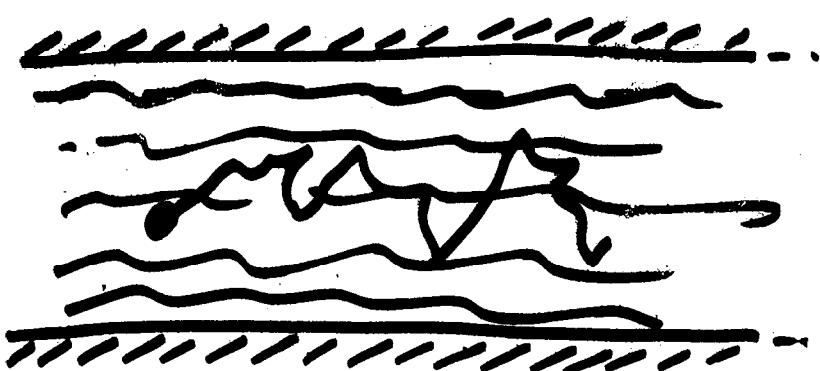
$$U_1 = A \sin x_3 + C \cos x_2$$

$$U_2 = B \sin x_1 + A \cos x_3$$

$$U_3 = C \sin x_2 + B \cos x_1$$



3. Instability and Class of Functions



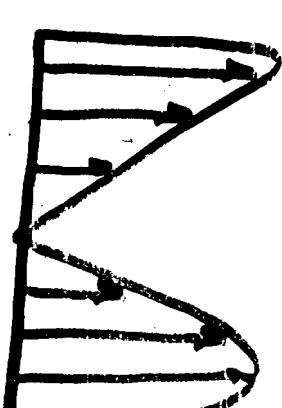
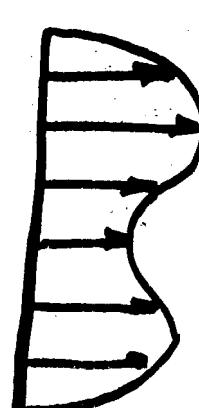
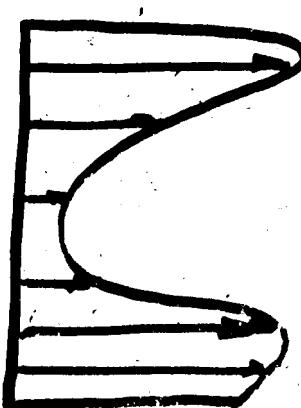
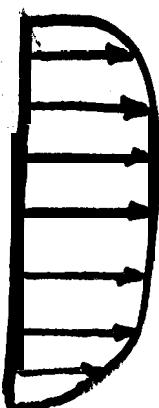
$$R > R_{cr}$$

$$\bar{v}_{av}$$

$$\sqrt{U^2}$$

$$\sqrt{W^2}$$

$$\sqrt{UW}$$



VISUALIZATION OF TURBULENT MOTION AND CHAOS

STABILIZATION PRINCIPLE

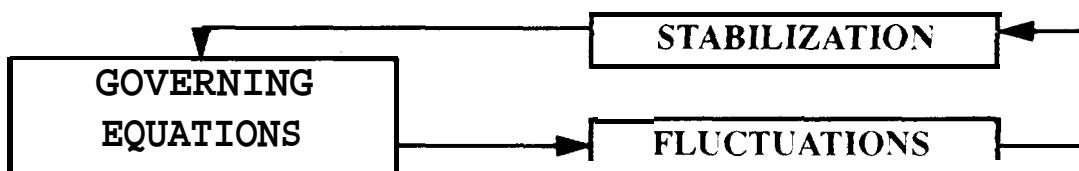
“The flows that occur in Nature must not only obey the equations of (fluid) dynamics, but also be stable.” — Landau

$$\frac{\partial v}{\partial t} + v \nabla v = - \frac{1}{\rho} \nabla p + v \nabla^2 v + \boxed{v \nabla v}$$

$$\nabla \cdot v = 0$$

$$\nabla \times v = 0$$

Choose $v \nabla v$ in such a way that the model is stable!



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Stabilization Principle

If

$$\lambda^+ > 0 \text{ at } \overline{x^i x^j} \equiv 0$$

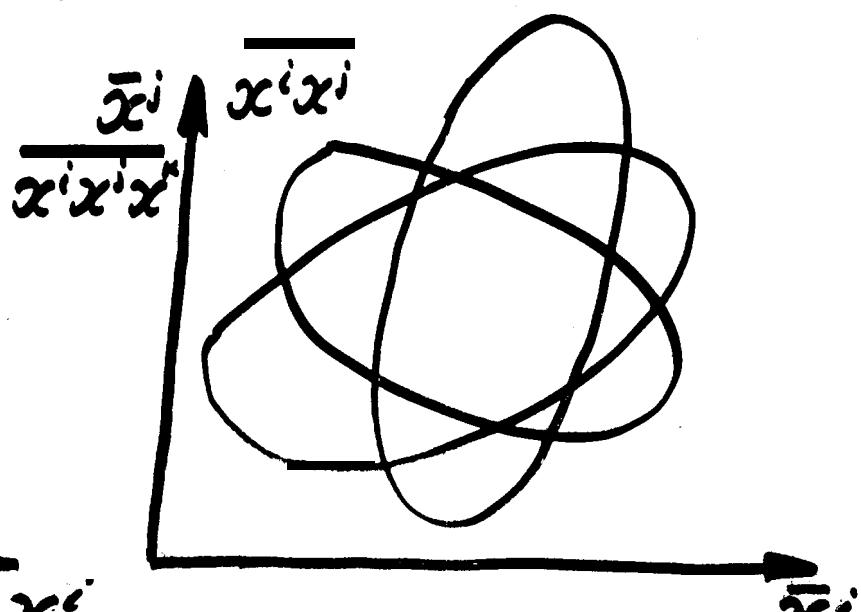
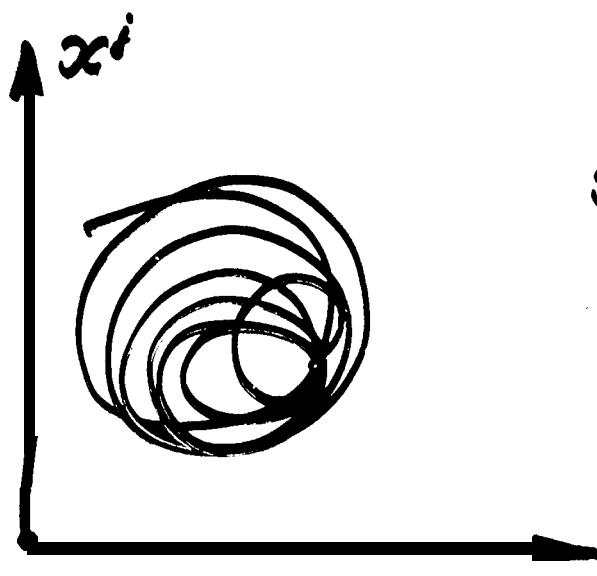
find $\overline{x^i x^j}$ from the condition

$$\lambda^+ = 0$$

$$\lambda^0 = \lambda^0$$

$$\lambda^- = \lambda^-$$

$$\overline{x^i x^j} = \varphi(x^*, \dot{x}^*, \dots \text{etc.})$$

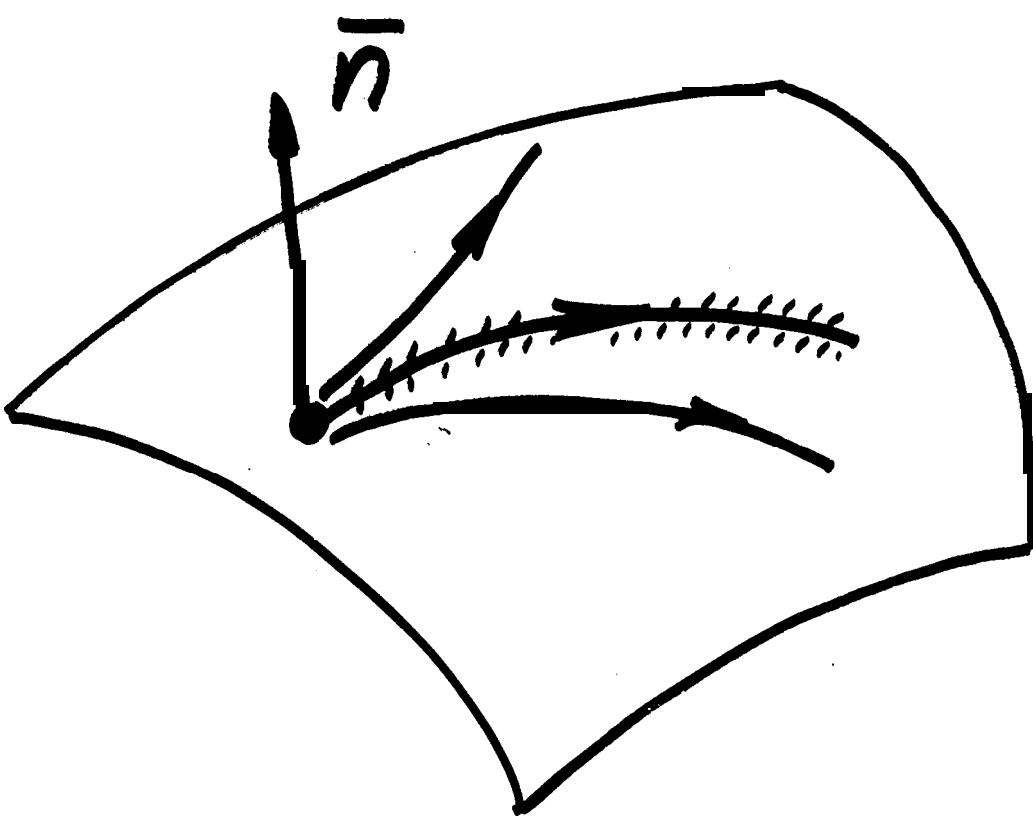


Example 2: Potential Motions

$$\ddot{g}^\alpha + \Gamma_{\beta\gamma}^\alpha \dot{g}^\beta \dot{g}^\gamma = - \frac{\partial \Pi}{\partial g^\alpha} + Q_{(i)}^\alpha, \quad Q_{(i)}^\alpha = - \frac{\partial \Pi_{(i)}}{\partial g^\alpha}$$

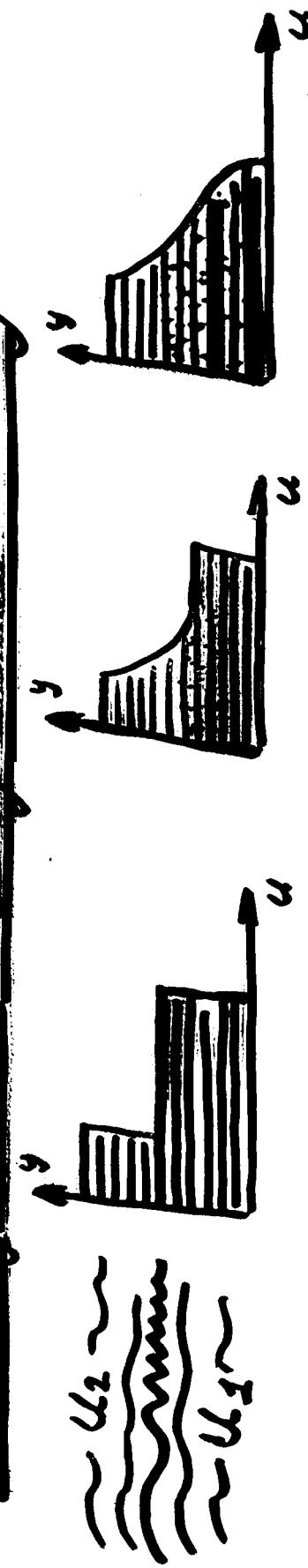
$$G + 3 \left[\frac{\nabla(\Pi + \Pi_{(i)}) \cdot \bar{n}}{2W} \right]^2 +$$

$$\frac{1}{W} \left[\frac{\partial^2 (\Pi + \Pi_{(i)})}{\partial g^i \partial g^j} - \Gamma_{ij}^\kappa \frac{\partial (\Pi + \Pi_{(i)})}{\partial g^\kappa} \right] n^i n^j = 0$$



$$W = \frac{1}{2} g_{ij} \dot{g}^i \dot{g}^j$$

Sine & cosine out off velocity discontinuity



$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + 2v \frac{\partial u}{\partial y} = \frac{1}{\rho} \frac{\partial \tilde{p}}{\partial y}, \quad C = -\sqrt{u' v'}$$

$$\bar{u}_1 = \bar{u}_1^0 - \frac{\sin [k(y-H)]}{\sinh(kH)} \left(\bar{u}_-^0 - \frac{1}{[Bak^2/\pi] \coth(kH)] \epsilon + 1/u_-^0} \right)$$

$$\bar{u}_2 = \bar{u}_2^0 + \frac{\sinh[k(y+H)]}{\sinh(kH)} \left(\bar{u}_+^0 - \frac{1}{[(Bak^2/\pi) \coth(kH)] \epsilon + 1/u_+^0} \right)$$

$$u_1'^2 + 2u_1'^3 = \frac{2ak \sinh[k(y+H)]}{\pi \sinh(kH) \tanh(kH)} \left(\frac{1}{[Bak^2/\pi] \coth(kH)] \epsilon + 1/u_-^0} \right)$$

$$u_2'^2 + 2u_2'^3 = \frac{2ak \sinh[k(y-H)]}{\pi \sinh(kH) \tanh(kH)} \left(\frac{1}{[(Bak^2/\pi) \coth(kH)] \epsilon + 1/u_+^0} \right)$$

Higher Order Approximations

$$\dot{x}_i = \alpha_{ij} x_j + \beta_{jmi} x_j x_m$$

$$\dot{\bar{x}}_i = \alpha_{ij} \bar{x}_j + \beta_{jmi} (\bar{x}_j \bar{x}_m + \bar{x}'_j \bar{x}'_m)$$

$$\dot{\overline{x'_i x'_k}} = \alpha_{ij} \overline{x'_j x'_k} + \alpha_{jk} \overline{x'_j x'_i} +$$

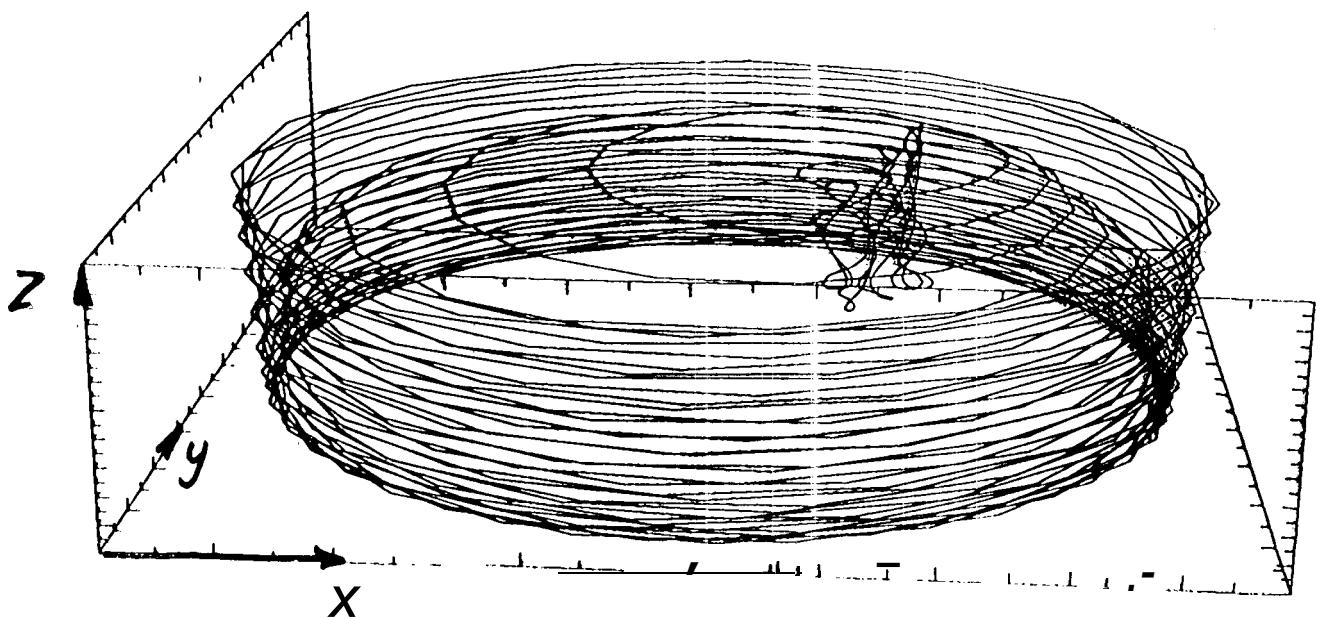
$$+ \beta_{jmi} (\bar{x}_j \overline{x'_m x'_k} + \bar{x}_m \overline{x'_k x'_j} + \bar{x}_k \overline{x'_j x'_m}) +$$

$$+ \beta_{jmk} (\bar{x}_j \overline{x'_m x'_i} + \bar{x}_m \overline{x'_i x'_j} + \bar{x}_i \overline{x'_j x'_m}) +$$

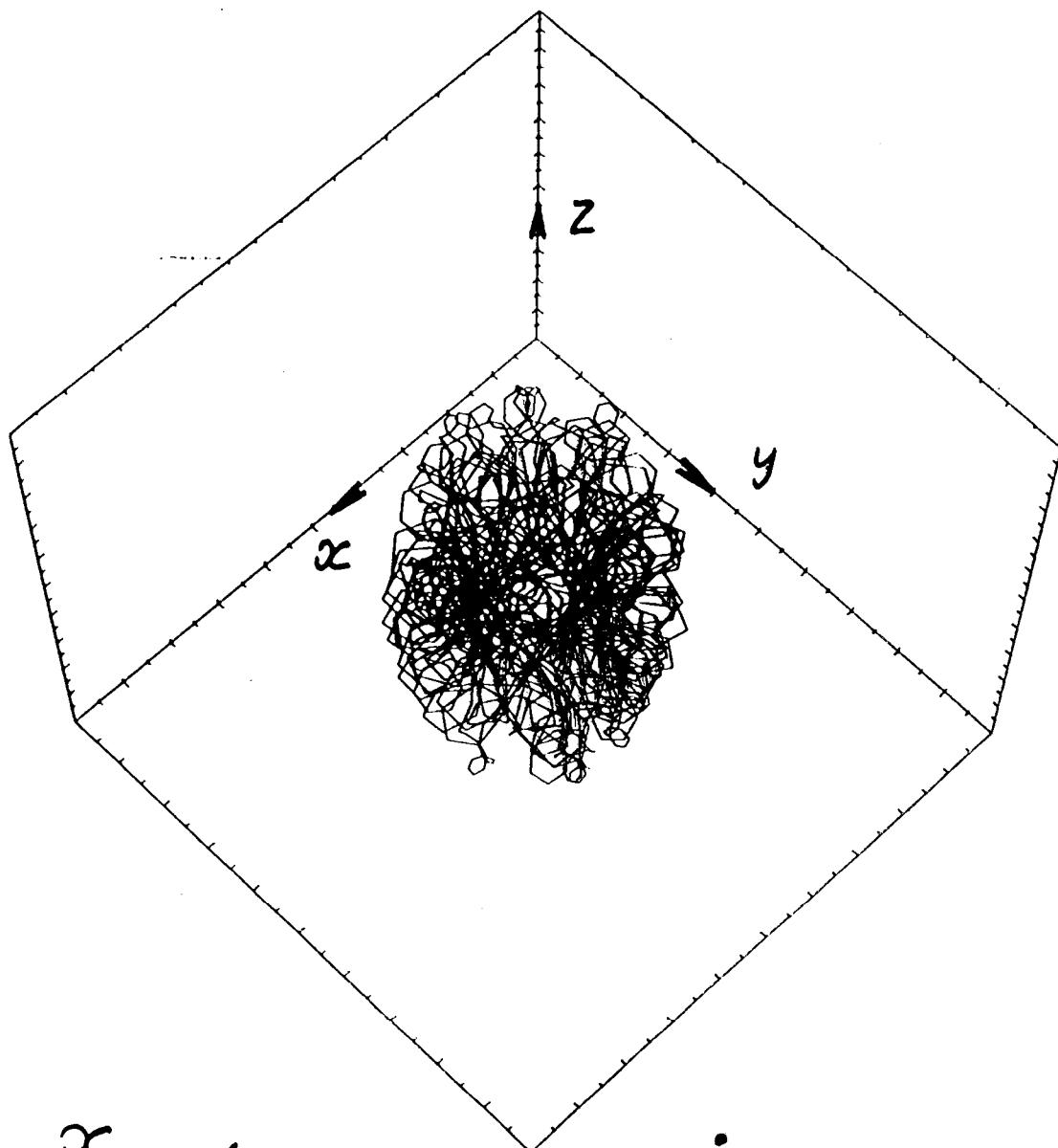
$$+ \beta_{jmi} \overline{x'_k x'_j x'_m} + \beta_{jmk} \overline{x'_i x'_j x'_m}$$

$$\begin{aligned}\bar{AB} &= \bar{A}\bar{B} + \bar{A}'\bar{B}' \\ A &= \bar{A} + A' \\ B &= \bar{B} + B'\end{aligned}$$

The Mean Motion



Charged Particle in a Uniform Magnetic Field



$$\dot{v}_x = -\frac{x}{\mu^3} - v_y$$

$$\dot{v}_y = \frac{y}{\mu^3} + v_x$$

$$\dot{v}_z = -\frac{z}{\mu^3}$$

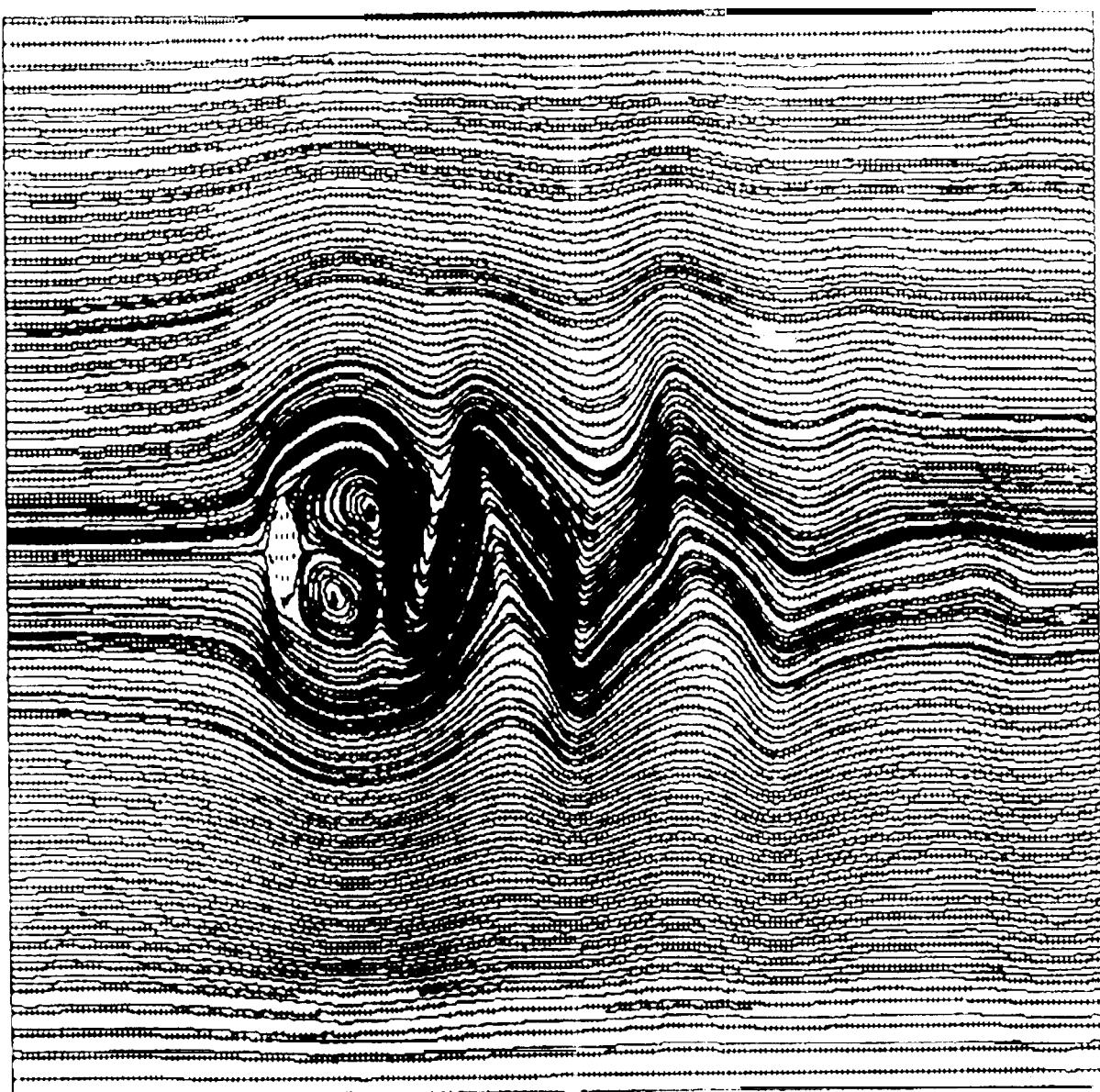
$$\dot{x} = v_x$$

$$\dot{y} = v_y$$

$$\dot{z} = v_z$$

$$r^2 = x^2 + y^2 + z^2$$

STABILIZED FLOW PAST CYLINDER $Re = 500000$



$T = 52$

R. Meyers, M. Zak, A. Zak

20 April 1994

ARMY RESEARCH LABORATORY

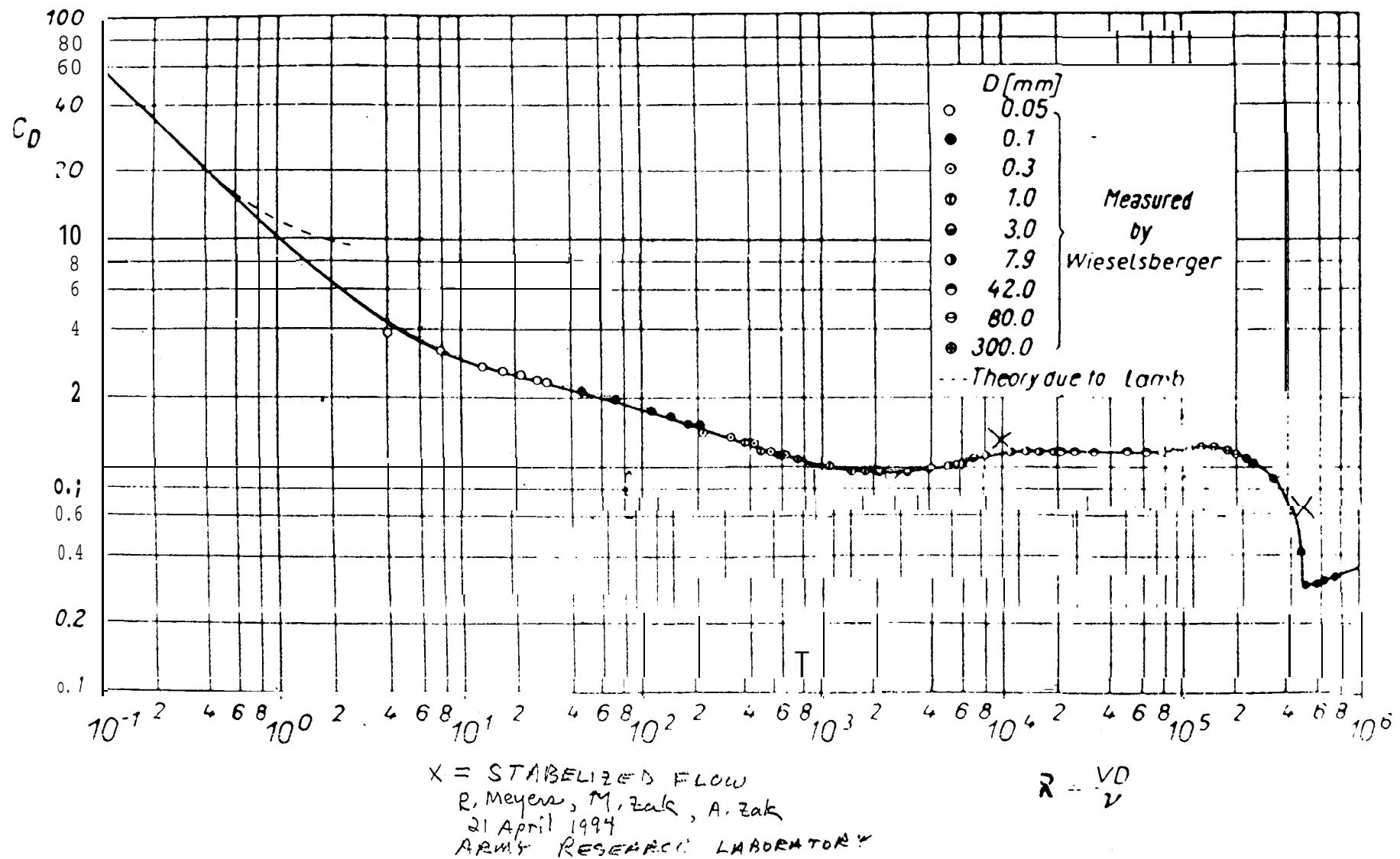


Fig. 1.4. Drag coefficient for circular cylinders as a function of the Reynolds number